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STUDIES ON FATIGUE BEHAVIOUR OF DISCONTINUOUS REINFORCED MMCs

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ABSTRACT

The objective of present article is to motivate the researchers in the field of fatigue behavior of discontinuous reinforced MMCs (DRMMCs). The DRMMCs, known for high strength, stiffness and fatigue life, are extensively used in many engineering applications such as aerospace, automobiles and hydrospace structures. The DRMMC structures shows the sound fatigue-resistant properties during the service period. Nevertheless, the evaluation of fatigue life of components well in advance is very important and challenging so that the maintenance/ replacement can be scheduled well before any catastrophic failure. The fatigue damage, a limiting factor for estimating the life of DRMMCs, is a complex metallurgical process involving the cyclic/recurring variable stress levels within the material, the area around reinforcements and the mismatch in the stiffnesses of constituents. The damage evolves successively from fatigue crack nucleation/initiation processes resulting into a short crack, followed by the long crack; ultimately, leading to the sudden failure of components.

Keywords: DRMMCs, Fatigue crack growth rate, Low-cycle fatigue; Fatigue life; Fatigue damaged

Introduction

The composites cover a large range of materials including the metal matrix, ceramic matrix, polymer matrix composites, elastomeric composites, etc. The metal matrix composites (MMCs) comparatively are matured enough for weight-sensitive and stiffness-critical components such as connecting rod, crankshaft, driving shaft, break rotor disk etc. [1-13]. The unique feature of MMC offers a plethora of industrial applications just by amalgamating various matrices and reinforcements [5, 8]. As with any other composites, the mismatch between coefficients of thermal expansion

of reinforcement and the matrix causes thermal residual stresses within the matrix of MMCs during the fabrication process [8, 14-34]. These stresses play a significant role on mechanical and physical properties of composite, like plastic yielding, failure of the material, etc. [35]. The thermal stresses can be relaxed by exploiting several mechanisms like interface debonding, micro-plasticity of metal matrix, and crack initiation and propagation [24].

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Why DRMMCs?

The MMCs are broadly classified into two groups based on microstructure: (i) continuously reinforced MMCs (CRMMCs) and (ii) discontinuously reinforced MMCs (DRMMCs) shown in Fig. 1. Schmidt in 1924 developed the first MMC using the mixture of aluminum/alumina powders [2]. During 1960s, the CRMMCs were used in the industrial applications due its high load bearing effect of the hard reinforcement without considering the microstructure and strength of the matrix; however, research on CRMMC declined during 1970s due to its high cost. In 1980s, DRMMCs were produced very fast due to their excellent properties such as high workability, low cost and significant increase in the mechanical properties over the metals. They were adopted in aerospace and automobile industries rapidly for its high strength-to-weight ratio, high specific modulus, high specific strength, excellent wear resistance, and thermal expansion coefficient as well as fatigue strength [2].

Market Demand of DRMMCs

In 1983, Toyota motor replaced the existing piston ring with aluminium based MMC (reinforced with 5% short fiber Al₂O₃) in the engine to prevent seizure. It was observed that wear is reduced four times, seizure stresses were doubled and weight was reduced by 5% to 10% as compared to Al alloy [36]. The automobile driving shaft made up of steel was replaced with AA6061-Al₂O₃-20p MMCs. The specific

strength of shaft increases from 26.6 km²s⁻² to 34.7 km²s⁻². As a result, the speed of shaft could increase up to 14%. The brake rotor discs made up of cast iron were replaced with Al-SiC-20p MMCs and observed good wear resistance and thermal stability [2, 37]. Recently market review [38] suggest that the demand of MMCs on global level is expected to increase from 5496 tons to 8000 tons during 2012 to 2019 as shown in Fig. 2.

Fatigue Behavior

Fatigue is an important property which causes under the cyclic and variable amplitude loading conditions. The cyclic loading results into damage and material property degradation in a cumulative manner [39]. The investigations on fatigue behavior of DRMMCs accomplished much recognition in late 1980s [40, 41] when researchers started its comparison with the metals; however, to the best of knowledge, very limited work is reported in the area of fatigue failure of DRMMCs. The continuous technological advancements explored the major factors, affecting the fatigue life of DRMMCs, such as stress levels within the material, area around the reinforcements, the mismatch in stiffness's and matrix locking stresses during the manufacturing/loading. The DRMMC structures have good fatigue-resistant properties during the service period. Moreover, it is required to calculate remaining life of these structures.

Catastrophic Failure

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There are many catastrophic failures of aerospace structures. In January 1954, the first jet propelled passenger airplane, Comet was crashed into the Mediterranean Sea. After the long investigations of its components it was concluded that the accident caused due to the fatigue failure of crew cabin leading to catastrophic failure of Aeroplan. In late 1960's, the brittle fracture was observed in the components of F-111 aircraft due to the pre-existing flaw that caused aircraft crashed catastrophically [39]. In 1967, the Point Pleasant Bridge was collapsed in the west Virginia without warning due to the cleavage fracture of an eye bar [39]. The best-known failure of a brittle ceramic matrix composite occurred when carbon-carbon composite tile on the leading edge of wing of the space shuttle Columbia fractured when impacted during the take-off. It led to catastrophic break-up of vehicle when it re-entered the earth's atmosphere on 1 February 2003. The high-strength steel rod that snapped on the east span of San Francisco-Oakland Bay Bridge also suffered from "fatigue failure" on October 28, 2009 [38].

FATIGUE BEHAVIOR OF DRMMCS

The fatigue damage, limiting factor for estimating the life of DRMMCs, is a complex metallurgical process involving the cyclic/recurring variable stress levels within the material, the area around reinforcements and the mismatch in the stiffness's of constituents [36]. The damage evolves successively from fatigue crack nucleation/initiation leading to the short crack followed

by the long crack and ultimately sudden failure of component [43-46]. The concept of fracture mechanics is used to evaluate the critical size of a crack [47-49]. Early fatigue crack growth life prediction models were based on the Linear Elastic Fracture Mechanics theory. In metals, the concept of cyclic plastic zone correlates the plastic strain amplitude with the fatigue crack growth [50-56]. The micro-structural features of DRMMCs play an important role in the evolution of fatigue damage. It has been established that the fatigue crack growth life of DRMMCs can be controlled by the micro-structural parameters such as particle size (or aspect ratio), reinforcement volume fraction, interfacial bonding strength, constraints of fiber in the matrix material, etc. [57-62]. The knowledge of strained controlled fatigue damage tolerance characteristics is required in order to have a better understanding of the fatigue behavior of DRMMCs.

Experimental and Theoretical Investigations
Numerous experimental and theoretical investigations have been carried out to understand the strain-controlled fatigue damage tolerance characteristics of DRMMCs [10, 36, 40-43, 58-60, 63-83]. It has been observed that the strengthening effect of hard reinforcement play a vital role in predicting the fatigue crack growth life of the DRMMCs [57-59, 61, 62]. Ding et al. [58, 59] proposed low cycle fatigue life prediction models based on the modified rule of mixture and strengthening factor of DRMMCs. To relate the microstructure with the macroscopic properties of DRMMCs,

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modified rule of mixture and strengthening factor theories were considered in the development of fatigue life prediction models. The results for aluminium based DRMMCs shows that micro-structural parameters have a significant effect on the fatigue life. These modeling techniques did not consider few micro-structural parameters such as reinforcement size, volume fraction, cyclic strain hardening exponent, cyclic strength coefficient and level of constraint in the crack-tip region that may affect the fatigue life of DRMMCs. Recently, Tevatia and Srivastava [84], developed an analytical model considering all the above said microstructural parameters.

Modelling of DRMMCs

Over the last two decades, a lot of fatigue crack growth life prediction models have been developed for estimating the fatigue life [46, 58, 59, 61, 62, 84-88]. Recently, an analytical model based on the complete fatigue damage evolution considering the micro-structural features of DRMMCs are developed [87]. McDowell et al. [45] established that the fatigue damage evolution in metals can be divided into four stages: (i) crack initiation/nucleation; (ii) short crack growth; (iii) physically short crack growth; and (iv) long crack growth, referred as multistage fatigue crack growth. Xue et al. [89] developed micro-structural based multistage fatigue life prediction model for aluminium alloy. Giang et al. [90] proposed multistage analytical model for predicting the fatigue life of forged M3:2 tool steel under HCF conditions.

Scope of research work

The fatigue analysis of DRMMCs offers a considerable scope for the research work. Some of the possible extensions in the work could be as follows:

1. The fatigue experiments may be performed for different combinations of DRMMCs such as aluminium/ magnesium with B4C and hybrid composite (one ductile matrix material with two ceramic reinforcement).
2. The effect of fiber orientation and fiber length size are not considered in the modelling because these two parameters are also important, and model may be modified considering these effects.
3. The present models are limited to the planar composite. The modeling can be extended to non-planar DRMMCs.
4. The analysis of surface crack of different shapes like ellipsoidal, oval, penny etc. may be carried out for estimating the fatigue crack growth life under the total strain-controlled condition.

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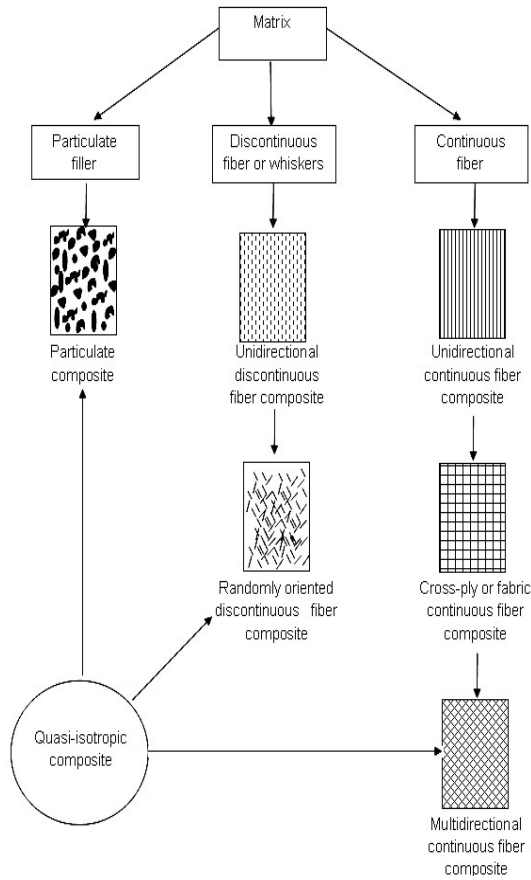
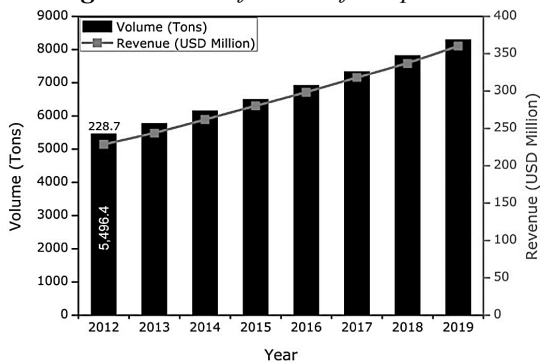


Figure 1: Classification of composite materials [9]



91. **Figure 2:** The global industrial demand of MMCs